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Fire resistance of additively manufactured water filled polymer parts.

H. Brooks, C. Wright, S. Harris, A. Fsadni

Abstract:

This paper introduces the concept of additively manufactured (AM) water filled parts (WFPs). By combining the energy absorbing properties of water with polymers it is possible to significantly improve time to ignition of AM parts with open internal structures. Theory relating the flame temperature to the maximum wall temperature of WFPs is developed. A range of water-polymer configurations are presented as a basis for WFP designs. Three separate thermal experiments were conducted to test different aspects of the WFPs. The time to ignition for cone calorimetry samples was extended 794% over plain photopolymers. Case studies were used to demonstrate the effectiveness of WFPs with complex shapes. The results of thermo-fluid finite element simulations showed good agreement with experimental observations and provide a useful tool for the evaluation and optimisation of WFP designs. The fire resistance of thin walled structures were found to be significantly improved by adding water. The water filling strategy was found to be more effective than adding intumescent coatings. Finally further work and recommendations are discussed.

Keywords: Additive manufacturing; fire resistance; water; polymer; heat transfer.

Highlights:

- A novel concept of water filled parts (WFPs) is introduced.
- The WFPs show excellent fire resistance.
- Thermo-fluid FEA modelling was shown to be useful in predicting WFP performance.

1. Introduction

1.1 Background

An important consideration for the use of additive manufactured (AM) polymers in high fire risk areas, is the polymers flammability and heat strength [1]. Of the 345 polymers listed on Senvol's additive manufacturing database only eight are currently rated V-0 according to the UL 94 standard [2]. The V-0 rated polymers are either high performance plastics (PEEK, PEAK, PEI or PPSF) or contain chemical flame retardants. Processing polymers with high thermal performance such as PEEK is more expensive than polymers like PA12, due to higher material costs, higher processing temperatures and low powder recyclability [3-6]. Polymers in general also suffer from fairly low heat deflection temperatures ranging from 38-263°C at 0.45MPa, a property not improved by adding flame retardants [2]. At 300-400°C most polymers begin to decompose releasing flammable volatiles which add further fuel to flames [7-11]. There is extensive research aimed at improving the flame retarding properties of polymers. This is done in three main ways: (i) developing inherently flame retardant polymers, (ii) chemically modifying polymers and (iii) adding flame retardant particles to polymers [12]. Polymers with flame retardants often require high particle loadings which can negatively affect the mechanical properties [13, 14], reduce recyclability and introduce harmful chemicals, such as halogens, into the environment [15-17]. Polymers used in AM have additional

constraints when considering adding flame retardants, as processing often requires a very narrow range of stock material properties, such as powder flowability, particle size distribution, heat absorption, polymer viscosity and the stability of colloids or suspensions in photopolymer resins [18, 19].

Another strategy to improve the fire resistance of polymers is to add a thermal barrier coating. A number of different coatings have been developed to insulate load-bearing substrates from fire using mineral refractories or intumescent materials [20]. They all function by forming a low density, air or gas-containing structure which achieves its thermal resistance by immobilising the gas within it. The thermal conductivity of such structures is generally of the order of 0.01–0.05 W/mK, regardless of the type of material [1]. While thermal barrier coatings are proven to be effective they are often not viable in many applications due to their added weight, low durability, appearance and solubility in water [21, 22].

This paper presents a simple, effective and environmentally benign method for improving the fire resistance of AM parts, without the use of specially formulated polymers or coatings, simply by filling them with water. These components will be referred to as water filled parts (WFPs). The concept is based on the well-known class room physics demonstration where a paper bag is filled with water and placed over a flame. The paper does not burn, not because it is wet, but because the water absorbs the heat keeping the paper below its ignition temperature.

1.2 Water filled parts (WFPs)

The concept of improving fire resistance by filling structures with water is not new and has been applied to large steel structures [23, 24]. Adding water to fire resistant fabric laminates has also been investigated via the addition of hydrogel layers [25]. This is believed to be the first study of its kind with a focus on the flame resistance of small complex polymer parts.

Polymers with low thermal conductivity and specific heat result in materials with surfaces that can rapidly increase in temperature when subjected to a heat source, such as a flame. Table 1 provides thermal conductivity and specific heat capacity data for some common materials. Note that water has a very high gravimetric and volumetric specific heat capacity. Water also has the benefit of being a fluid at room temperature, capable of high convective heat transfer and has a large latent heat of vaporisation. All of these properties make water an excellent choice to combine with polymers to improve the fire resistance of the printed parts.

Table 1. Thermal conductivities and specific heats of common materials.

Material	Thermal conductivity at 25°C (W/m K)	Specific heat capacity	
		(J/kg K)	(J/m ³ K)
PA 6	0.25	1600	1824
PLA	0.13	1800	2340
Air	0.024	1005	1231
Wood (oak)	0.17	2000	1833
Steel	43	490	3822
Aluminium	205	870	2484
Water	0.58	4182	4190
Concrete	1.7	880	2122

Understandably, water cannot be mixed into the polymer before printing so space must be made inside the part for the water at the design stage. Most polymer AM technologies are capable

of producing hollow parts with open internal structures that provide space for the water. For powder bed fusion, vat polymerisation and material extrusion methods these porous structures can then be filled with water in a post-build process and subsequently sealed (Figure 1a). It may also be necessary to make the polymer part watertight before adding the water by coating with a sealant [26, 27]. Material jetting technologies can be used to print the polymer and water simultaneously [28], avoiding the need for a two part process and allowing isolated and functionally graded internal volumes of water (Figure 1b). For thick parts where weight reduction is a concern a double shell structure can be used, as shown in Figure 1c. If the surface of the part is likely to be damaged then multiple shells may be added for redundancy. It is also possible to combine different strategies to find the right combination of strength, durability and weight.

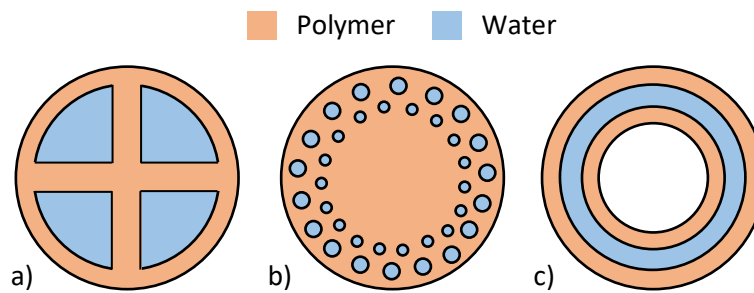


Figure 1. Cross sections of three water/polymer configurations: a) A hollow or open lattice structure filled with water, b) Functionally graded water volumes, c) double shell structure with water trapped between the inner and outer polymer shells.

Another important design consideration is the build-up of pressure within WFPs as the water is heated. Many polymers will soften sufficiently at 100°C such that a thin wall (less than 1 mm thick) will leak at relatively low pressures. For thick walled parts with softening temperatures over 100°C it may be necessary to include pressure relief points designed to preferentially vent when internal pressures start to rise above unsafe levels.

1.3 Heat transfer theory

Instantaneous heat transfer across a polymer wall, involves both convection and conduction as described by Equation 1. As heat transfers through the wall the water will increase in temperature until it reaches 100°C.

$$\dot{Q} = \frac{A}{\left[\frac{1}{h_h} + \frac{t_p}{k} + \frac{1}{h_c}\right]} (T_h - T_c) \quad \text{Equation (1)}$$

A = the wall surface area, h_h = the effective convective heat transfer coefficient on the hot side, t_p = the wall thickness, k = the polymer conductivity, h_c = the convective heat transfer coefficient on the cold side, T_h = Temperature of the hot side, T_c = Temperature of the cold side.

The convective heat transfer coefficient on the water side is highly temperature dependant and varies between surfaces with different material combinations, surface roughness and local geometries. To simplify this problem the water can be assumed to be 100°C until the water has completely converted to steam. The high temperature of the water is compensated for by the

extremely high convective heat transfer rates present during boiling. If this assumption is made the problem becomes static and the heat transfer and wall temperatures do not change with time.

The temperature of the wall surfaces is related to the temperature difference between the flame, water, and the heat flow described by Equation 2.

$$T_h - T_c = (T_h - T_{hw}) + (T_{hw} - T_{cw}) + (T_{cw} - T_c) = \frac{\dot{Q}}{A} \left[\frac{1}{h_c} + \frac{t_p}{k} + \frac{1}{h_h} \right] \quad \text{Equation (2)}$$

where T_{hw} = the hot side wall temperature, T_{cw} = the cold side wall temperature.

Of critical importance is the maximum temperature of the polymer wall, T_{hw} . This can be calculated via Equation 3.

$$T_{hw} = T_{cw} - (T_{cw} - T_h) / \left(\frac{h_c}{h_h} + \frac{t_p h_c}{k} + 1 \right) \quad \text{Equation (3)}$$

Assuming values for the heat transfer coefficients, polymer conductivity, flame temperature and water temperature, it is possible to investigate the effect of wall thickness and water temperature on the temperature profile across the polymer wall.

Table 2. Values used in Equations 1 - 3 to generate Figures 2 and 3.

Parameter	Value	Units
t_p	0.5×10^{-3} to 2×10^{-3}	m
k	0.2	W/mK
h_h	54.3	W/m ² K
h_c	$= 20(T_c) + 500$	W/m ² K
T_c	273 to 373	K
T_h	2026	K
A	1	m ²

The values for h_h and T_h were adopted from the work of Wang *et al.* [29, 30] to represent the effective heat transfer coefficient and temperature of a flame consistent with UL 94 standards. The value for k was chosen as a mid-range value for polymers. A linear relationship for h_c was assumed, based on commonly quoted values for the convective heat transfer of water at 20 and 100°C. Figure 2 shows the temperature profile across polymer walls of varying thicknesses for a water temperature of 100°C. While the inside wall is maintained near 100°C for all thicknesses the outside wall temperature is almost linearly related to the wall thickness. For the 0.5 mm and 2.0 mm walls the maximum temperature is calculated to be 325°C and 697°C respectively.

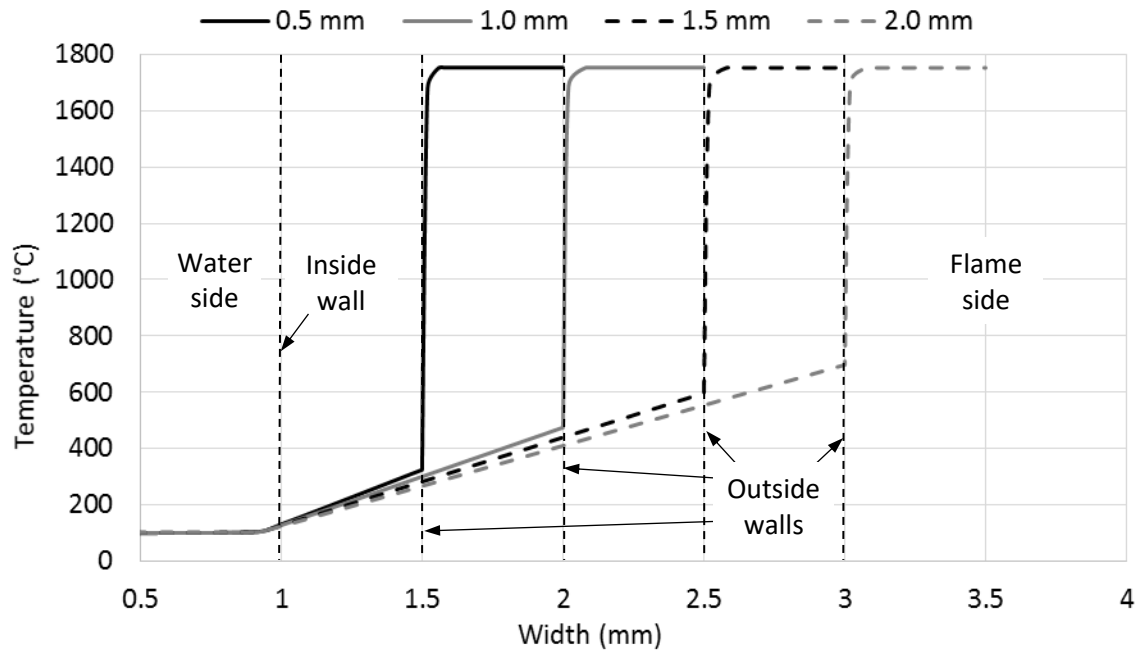


Figure 2. Temperature profiles across different polymer wall thicknesses for water at 100°C.

Using the same equations it is possible to determine the effect of water temperature on the maximum wall temperature. The temperature profiles for 0.5 mm thick walls are shown in Figure 3, revealing that the water temperature has little influence on the maximum polymer temperature. Surprisingly when the water is at 0°C the flame-side of the wall is slightly hotter than when the water is 100°C. This is due to the fact the convective heat transfer of naturally convecting cold water is much lower than that of nucleate boiling water [31, 32].

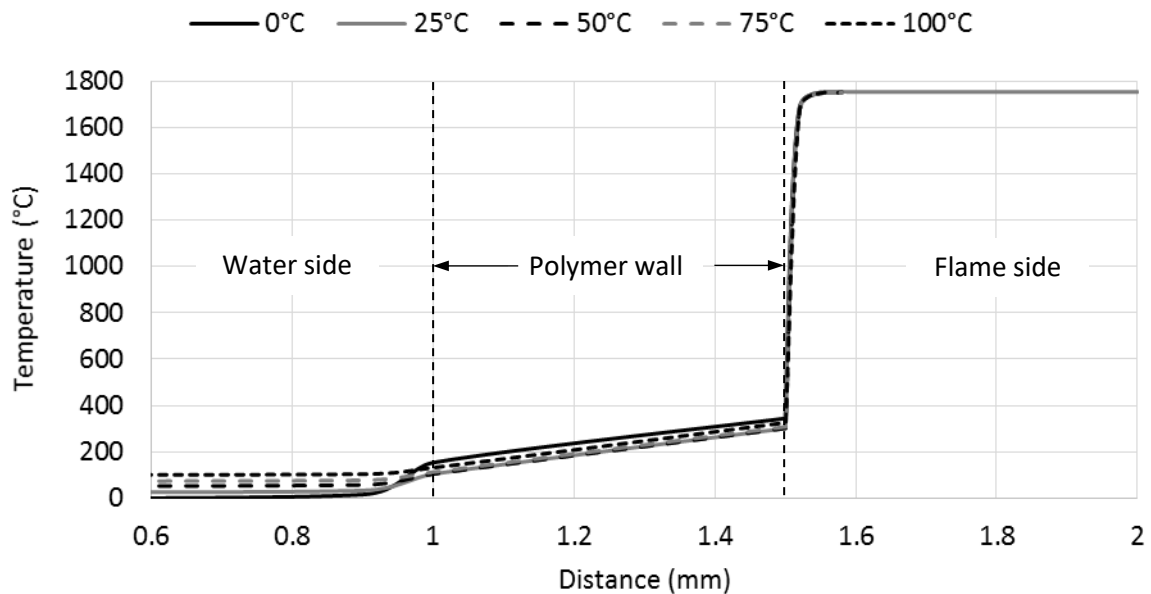


Figure 3. Temperature profiles for a 0.5 mm thick polymer wall with different water temperatures on the cold side.

The equations also show the heat flow across the wall is inversely related to the wall thickness. This means that while thin walls lead to lower maximum wall temperatures the water will boil faster. The theory presented here provided initial estimates for the effective wall thicknesses used in the following studies.

2. Experimental Method

Three primary experiments were conducted to test different aspects of the WFPs. Cone calorimetry was used to assess how the WFPs coped with a radiant heat source from above and to determine how the heat release rate and smoke production rate are effected. The final two experiments were case studies: Case study 1 was aimed at investigating how the water affects a cantilevers ability to hold a load whilst being in contact with a flame. Case study 2 investigated if a relatively thin walled part with local features of high polymer to water ratio, can also be improved using this concept.

All samples were printed using a Formlabs Form1+ SLA printer and clear methacrylic photoactive resin (GPCL02) with 0.1 mm layer heights. The as-printed samples were left on a window sill for a day to post cure. As this curing method is known to be inferior to UV curing the properties are likely to be closer to the green part properties shown in Table 3.

Table 3. Material properties for Formlabs clear resin (GPCL02) [33].

Property	Green	Post cured	Method
Tensile strength at yield	29.8 Mpa	61.5 MPa	ASTM D 638-10
Young's modulus	1.3 GPa	2.7 GPa	ASTM D 638-10
Heat deflection temp. at 0.455 MPa	325 K	351 K	ASTM D 648-07
5% weight loss temperature	520 K	547 K	ASTM E 1131

Specific sample geometries are given in the following sections. The clear material allowed the initiation of boiling to be visually observed. For improved readability the results and discussion of each test will immediately follow the relevant methods section.

2.1 Cone Calorimetry test

2.1.1 Method

The cone calorimetry test was carried out in accordance with BS ISO 5660-1:2015 with an irradiance set at 35 kW/m² (702°C) 50mm below the cone heater in order to measure the heat release rate, time to ignition and smoke production of the WFPs. The standard sample geometry was modified to allow a hollow internal cavity. 1 mm diameter support columns were added to improve the compressive strength of the samples during handling (Figure 4). Whilst samples in this test would normally be solid the WFPs are considered as metamaterials or polymer/water composites. Four holes were left in the shell to allow uncured resin to escape and were later sealed with hot melt adhesive. The tests were carried out in duplicate with two as-printed samples and two water filled samples.

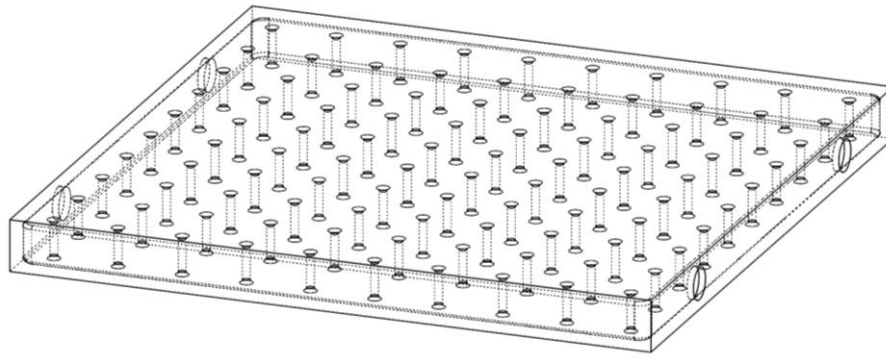


Figure 4. Cone calorimeter test samples, 100 x 100 x 8 mm with 1 mm thick shell and 1mm diameter support columns spaced at 5 mm intervals.

2.1.2 Results and discussion

The average results of the cone calorimetry tests are summarised in Table 4. The time to sustained ignition for the water filled sample was 8 times longer than the unfilled sample. This test confirms that the cooling effect of the water is effective even when the heat is radiated from above and there is less benefit from convective heat transfer within the water volume.

Table 4. Average cone calorimetry results for samples with and without water.

	Without water	With water
Time to sustained ignition (s)	32	283
Peak rate of heat release (kW/m ²)	483	452
Post ignition smoke production (m ² /m ²)	442	269

Once the majority of the water evaporated the water filled samples proceeded to burn with a similar intensity to the unfilled samples as shown by the heat release curves in Figure 5.

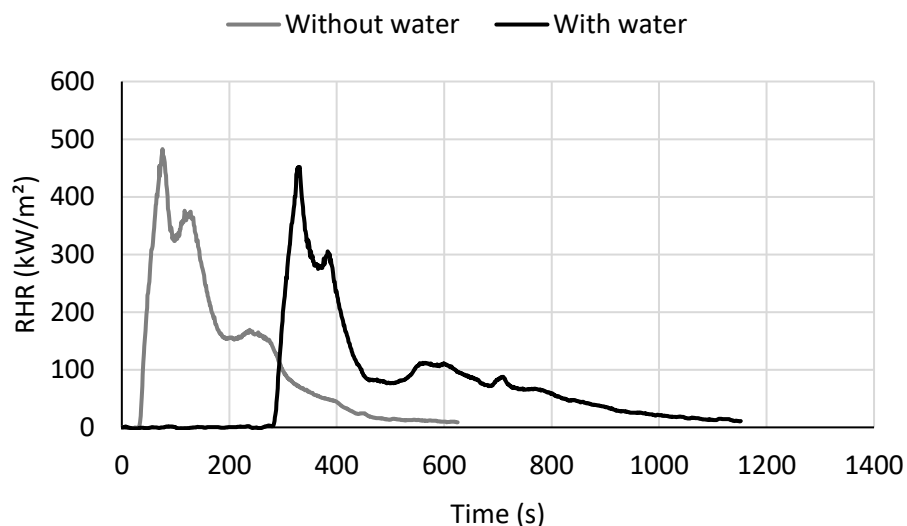


Figure 5. Rate of heat release for samples with and without water.

The maximum smoke production rate for the water filled sample was significantly lower than the unfilled sample and delayed by approximately 250 seconds (Figure 6). The total post

ignition smoke production for the unfilled sample was measured to be 65% greater than the water filled sample.

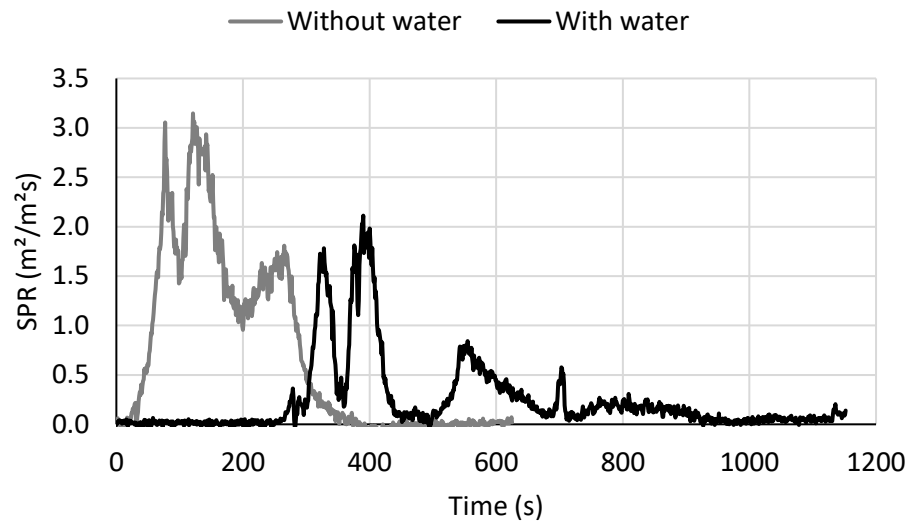


Figure 6. Smoke production rate versus time for samples with and without water.

Smoke production is analysed by measuring how the smoke attenuates a laser beam in the exhaust duct. The attenuation is related to volume flow, resulting in a measure of smoke density. It is unclear at this stage why the smoke production for the water filled sample was diminished. It is possible that, water vapour condensed in the exhaust duct, captured particles that would otherwise have attenuated the laser beam.

2.2 Case study 1 – Load bearing cantilever

Case study 1 was designed to test how WFPs will perform when subjected to both thermal and mechanical loads.

2.2.1 Method

Five cantilever designs were trialled. In all cases only the internal volume of the cantilevers was allowed to be altered. This was to reflect real world constraints that may reduce design freedoms. Figure 7 shows the overall shape of the cantilevers along with the five unique internal structures. The designs were chosen to cover the range from fully solid cross sections to completely hollow, with a range of intermediate structures in between.

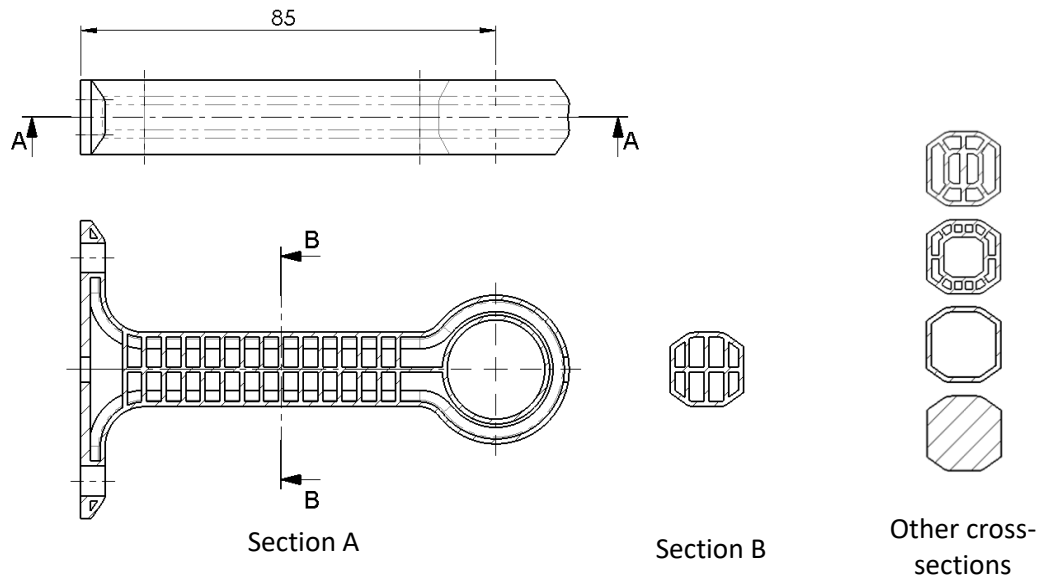


Figure 7. Design of the cantilever specimen for the heat deflection case study. The basic structure of the lattice design (L) is shown on the left. On the right are cross sections of the four other designs from top to bottom: Large shell (LS), Small shell (SS), Hollow (H) and Solid (S).

The two shell designs (LS and SS) each contained two discrete internal volumes so that it was possible to fill only the outer volume with water. The average weights of each of the designs (with and without water) is shown in Table 5 below. Approximately 1 gram of glue was used to seal each sample. The WFPs are slightly lighter than the solid samples.

Table 5. Weights of the cantilever samples with and without water.

	As printed (g)	Water filled (g)	Water mass (g)
Solid (S)	26	NA	0
Hollow (H)	10.3	23.7	12.4
Lattice (L)	11.1	24.2	12.1
Large shell (LS)	14.1	22.3	7.2
Small shell (SS)	14.3	20.3	5.0

The first set of samples were loaded until failure at room temperature using calibrated weights to assess the relative strengths of the designs. These samples were not water filled. All tests were carried out in duplicate and the results averaged. To test the heat strength of the five designs a 50 W flame was applied to the straight section of the samples whilst supporting a 70 g load. For samples H and S, the vertical deflection was recorded over time (Figure 8). Additionally an H sample was given an intumescent coating (consisting of sodium silicate and milled carbon fibre in a volumetric ratio of 10:1) to see how thermal barrier strategies compare with the WFPs. The milled carbon fibre was found to improve the durability of the coating and ease application.

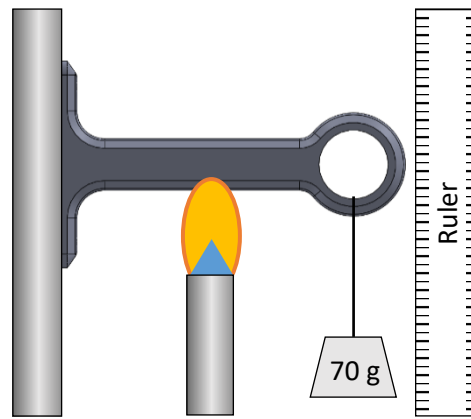


Figure 8. Experimental setup for the heat deflection case study.

2.2.2 Results and discussion

The results of the mechanical load tests showed the solid sample was approximately seven times stronger than WFP designs (Figure 9a). This is to be expected as the necessary thin walls of the WFPs significantly reduce the second moment of area of the samples. Internal support structures proved to have little influence on the ultimate strength of the WFPs compared to the completely hollow sample. The flame tests showed the water filled samples had significantly increased time to sustained ignition compared to the unfilled samples (Figure 9b). The water filled H and L designs failed due to softening of the polymer before they had a chance to ignite. The S, LS and SS designs all eventually caught fire before failing. Whilst the solid sample caught fire relatively early it took 228 seconds to fracture. It was interesting to note that the cantilever samples were much more fire resistant than the equivalent (1 mm thick walled) UL 94 samples. This was clearly due to the absence of sharp corners and edges in the cantilever design.

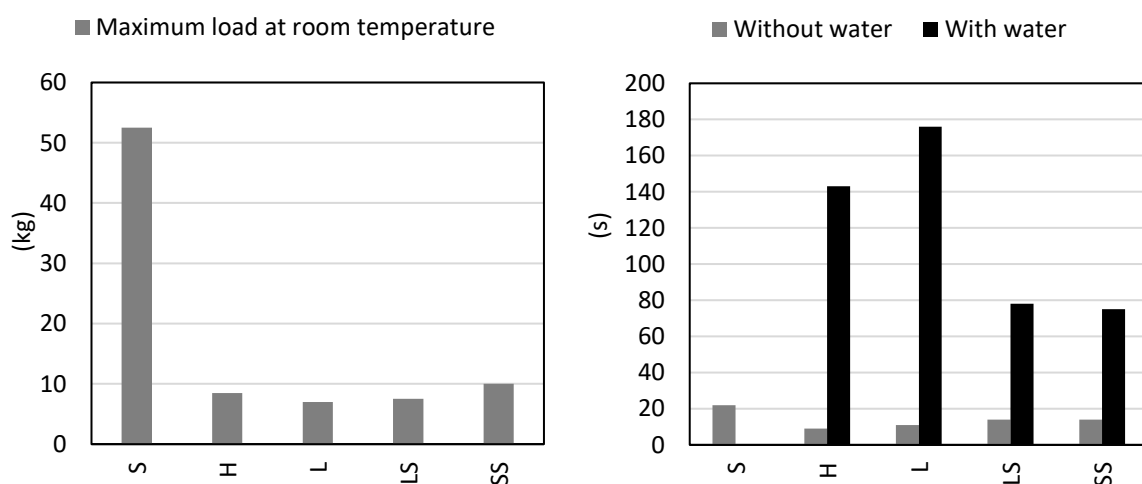


Figure 9. a) Average load at failure for cantilever designs at room temperature. b) Average time to sustained ignition for samples with and without water. Note: The water filled H and L designs failed before sustained ignition.

A key result of the flame tests is that if the flame had been removed after 60 seconds all of the WFPs would have survived. Additionally, if the flame was removed after 120 seconds the H and L water filled samples would have survived. Figure 10 shows the deflection of selected samples during

the flame tests. The dry hollow sample ignited and failed very quickly. The intumescent coating was found to delay failure of a dry hollow sample only slightly. The solid sample ignited early but was sufficiently strong to outlast the hollow sample with the intumescent coating. The two water filled samples took the longest to ignite and to fail. Clearly the water filled and coated sample was able to withstand the direct application of the flame the longest.

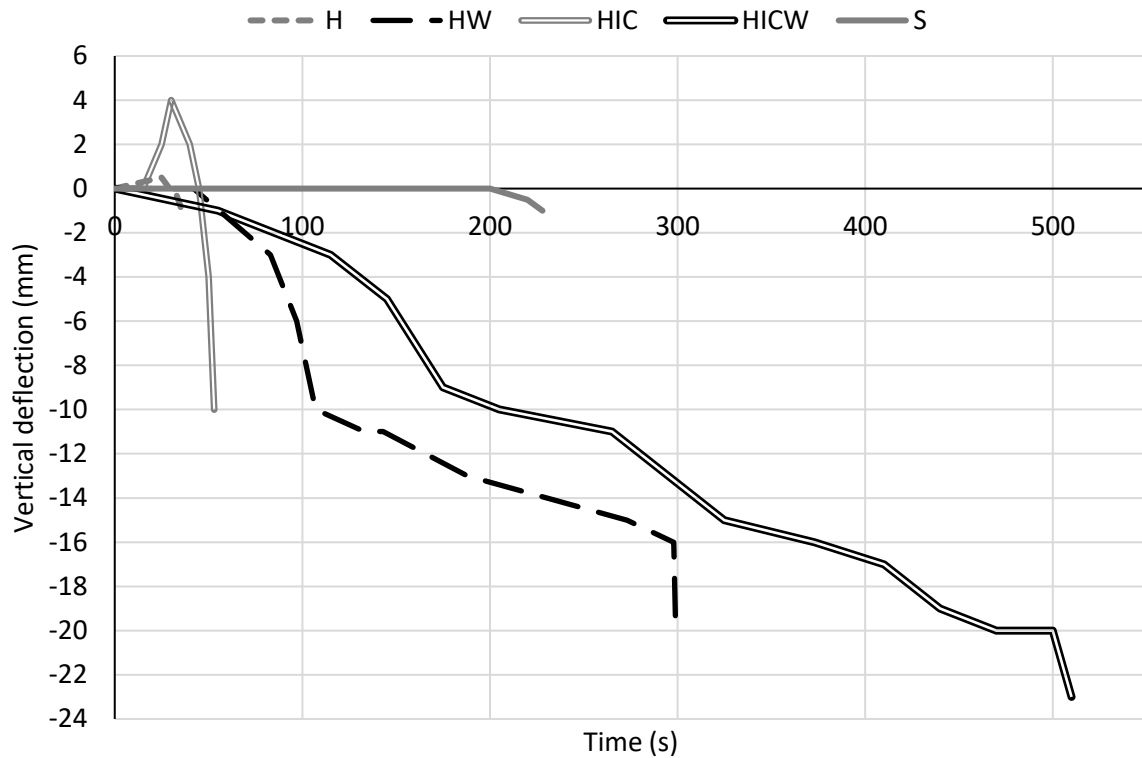


Figure 4. Vertical deflection of weighted cantilever samples with an applied flame. H (hollow), HW (hollow with water), HIC (hollow with intumescent coating), HICW (hollow with water and intumescent coating) and S (solid). Deflection measurements are within ± 1 mm.

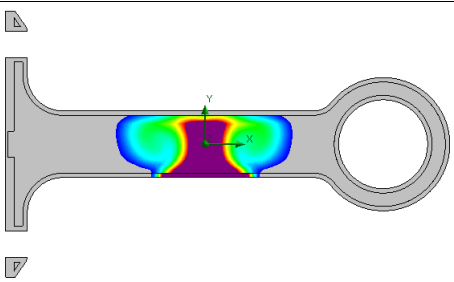
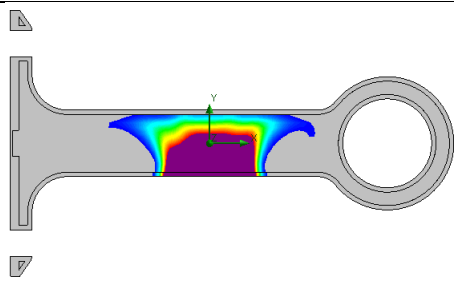
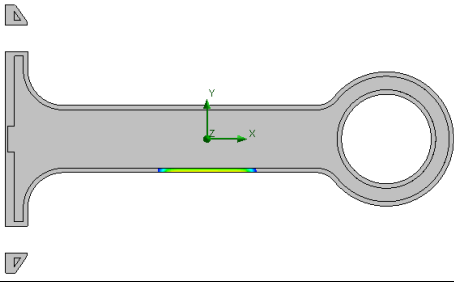
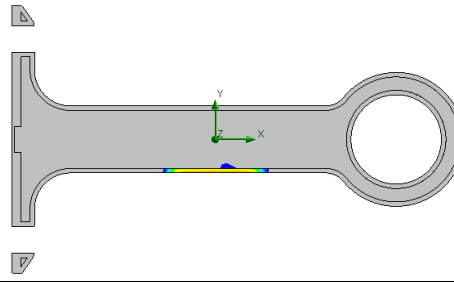
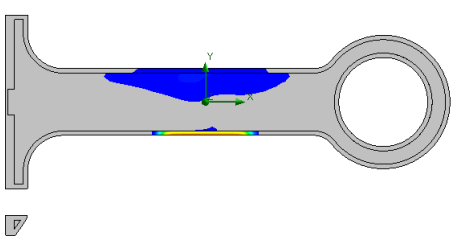
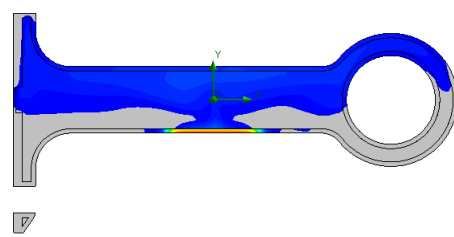
2.2.2.1 Thermal modelling

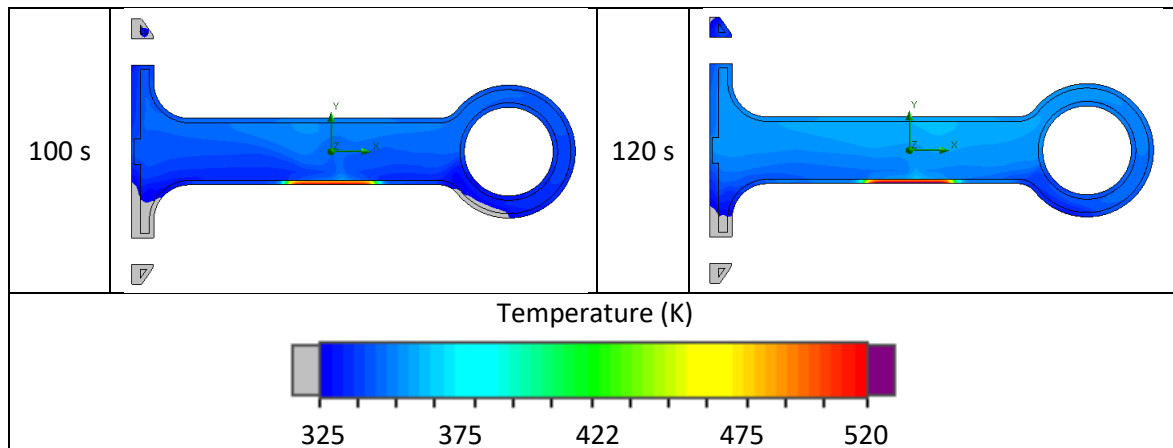
In order to understand the deflection characteristics of the hollow samples, finite element analysis (FEA) was used to simulate thermal conduction through the polymer walls and the subsequent internal convective fluid flow. Due to the lack of specific material property data for the cured resin, generic (mid-ranged) material property data for poly(metha methacrylate) (PMMA) was used. Specifically 0.2 W/mK, 1.18 g/cm³ and 1466 J/kgK for the thermal conductivity, density and specific heat capacity respectively. The material properties for air and water were taken without modification from the material library. The outer walls were assumed to be adiabatic whilst the heat from the flame was modelled by applying a heat transfer coefficient of 54.3 W/mK and a flame temperature of 2026 K to the bottom 10 mm of the sample, based on the findings of Wang *et al.* [29, 30]. The outer walls were assumed to be adiabatic whilst the heat from the flame was modelled by applying a 54.3 W/mK heat transfer coefficient and a flame temperature of 2026 K across a 20 mm wide section on the bottom surfaces. The 20 mm width is an estimate of the flame spread arrived at from experimental observation. The side walls directly above the flame were also given a 54.3 W/mK heat transfer coefficient with half the flame temperature (1013 K). The aim of the simulation was to model the warming phase and not boiling or combustion, hence the simulation of the water filled sample was stopped once the average water temperature reached 373.15 K. The hollow (dry)

simulation was stopped after 15 seconds. The time steps were set to 1 second for the water filled simulations and 0.5 seconds for the air filled simulation as further reductions in time step did not significantly change the results in either case. Automatic refinement of the mesh for solid cells and for narrow channels was enabled.

Table 6 presents a series of cut plots showing the temperature along the central plane of the cantilever at various times. The colour scheme was chosen to best display the progression of critical polymer temperatures throughout the part over time. The heat deflection temperature (ASTM D 648-07) at 0.455 MPa for the resin used in the experiments is 325 K for green parts and 351 K for parts post-cured with UV light [33]. The 70 g weight used in the experiment produces a maximum stress in the cantilever of 0.45 MPa (determined by static FEA at room temperature) which means the heat deflection temperature provided is comparable. The SLA parts used in the experiments were cured in sunlight as opposed to UV light and so are likely to be closer to the green material properties presented in Table 3.

Table 6. Cut plots showing the distribution of temperature from 325K (blue) to 520 K (red). Gray areas are under 325 K and purple areas are over 520 K.

Time	Temperature distribution	Time	Temperature distribution
Hollow design without water			
5 s		15 s	
Hollow design filled with water			
10 s		40 s	
50 s		70 s	



The simulations provide a very useful indicator of how the parts heat up over time. For the unfilled simulation it is clear that after 15 seconds a significant volume of polymer at the flame location is above the 5% weight loss temperature of 520 K. This relates well with the known ignition time of 9-18 seconds. For the water filled sample the proportion of material above the heat deflection temperature of 325 K increases dramatically between 50 and 100 seconds. This correlates well with the rapid increase in deflection seen in the experimental test.

The results demonstrate that thermo-fluid simulations are an effective tool for understanding the ignitability and warming characteristics of WFPs. Coupling the thermo-fluid simulation results with a mechanical analysis could allow the prediction of deformation and stress overtime.

2.3 Case study 2 – Thin walled object

For WFPs to be widely applicable it is important to know whether it is possible to improve the fire resistance of thin parts. There are many situations where the thickness of the parts may be limited, reducing the total volume available for water and greatly reducing local water:polymer ratios.

2.3.1 Methodology

A 40 mm computer fan housing was redesigned as shown in Figure 11.

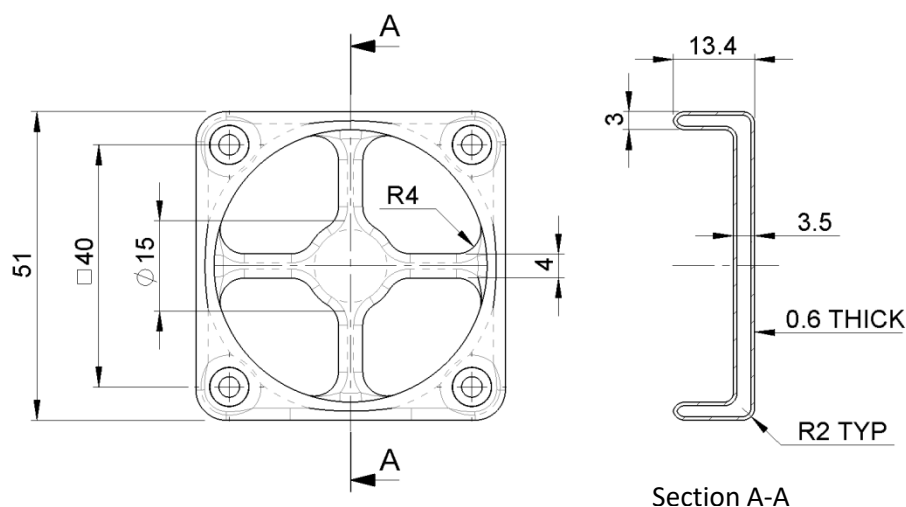


Figure 5. Design of the shelled 40 mm computer fan housing for case study 2.





The functional dimensions of the housing were unchanged while the wall thickness was increased from 1.5 mm to 3.5 mm and shelled with 0.6 mm walls. Four samples were printed, one was left as printed, one was filled with water, one was coated with an intumescent coating and one was filled with water and coated.

The fans were tested in the vertical orientation with a 50 W flame centred 10 mm below the part. The time to boil and time to ignition was recorded for the water filled sample.

2.3.2 Results and discussion

Both of the water filled samples had significantly longer times to sustained ignition than the unfilled samples. Unsurprisingly the water filled and coated sample survived direct contact with the flame the longest. A summary of the results are shown in Table 7.

Table 7. Results of computer fan housing case study.

	Housing without water	Coated housing without water	Water filled housing	Water filled and coated housing
Photos taken 11 seconds from the first application of the flame.				
Time for boiling to start (s)	N/A	N/A	67	Unknown
Time to ignition (s)	7	60	242	400

For the water filled sample 28% of the time to ignition was spent heating the water to boiling point. The rest of the time was spent evaporating the water before ignition could take place. This case study demonstrates that even very thin sections may significantly benefit from internal water cooling providing the fluid is free to move within the part. An additional finding is that the part should be designed with the preferential leak point located near the top of the part so that the water cannot escape due to gravity until it is converted to steam.

3. Conclusions

This paper introduced the concept of water filled parts (WFPs). By combining the energy absorbing properties of water with polymer parts it is possible to significantly improve the time to ignition. The technique may also be applied to rotation moulded parts and other manufacturing methods that allow the production of hollow shells. Additive manufacturing is particularly appropriate as it allows open internal lattices to be printed which can significantly increase the part

strength. In practice it was found that polymer walls approximately 1 mm thick provided a good compromise between strength and fire resistance as long as sharp corners were avoided.

The time to ignition for cone calorimetry samples (where the radiant heat source comes from above) was significantly extended. Measurements showed smoke production was reduced by half, although this result needs further verification. Case studies were used to demonstrate the effectiveness of WFPs with complex shapes. The fire resistance of thin walled structures was also found to be significantly improved, as long as the small water cavity near the flame was connected to water elsewhere in the part. The cantilever case study showed that the WFPs are significantly weaker than solid parts due to the bending stresses being highest in the thin outer walls. This will limit the usefulness of WFPs in many applications. A factor that goes some way to mitigate this problem is that many functional AM parts are already deliberately printed with sparse internal structures to increase build speed and reduce materials cost. The results of thermo-fluid finite element simulations showed good agreement with experimental observations and provide a useful tool for the evaluation and optimisation of WFPs. WFPs were compared with samples with intumescent coatings and the results indicate that WFPs delay the time to ignition more effectively than intumescent coatings.

For brevity the authors have only presented the results based on photo-polymerised resin parts however similar results for the cone calorimetry tests were seen with extruded PLA and laser sintered PA6 WFPs. It is likely that other high performance polymers such as PEEK or PPSF would also benefit from integrated internal water volumes. Whilst the fire resistance of WFPs has been validated there are still questions surrounding part durability, polymer degradation, biological contamination, cost and the best method for sealing the parts. Durability could be improved by maximising wall thickness and the internal lattice structures. Material jetting could provide a higher resolution water distribution allowing functionally graded water volumes within parts. Additional redundancy could be possible by implementing multiple discrete cavities in an onion layer structure. Biological inhibitors will be needed to prevent the growth of bacteria, viruses, protozoans and mould. Adding graphite powder, nanoparticles or other flame resistant thermally conductive materials to the water may improve performance by increasing heat transfer and providing additional fire resistance once the water has evaporated. Polymers which degrade in the presence of water should be modified or avoided where long life is required. Hydrogels may be a suitable replacement for water, reducing the chance of premature leakage.

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